

40 3 stage Rocket-

	stage 1	stage 2	stage 3
$m_s$	6,98,390	69,840	21,950
$m_p$	47,61,750	698,400	69,480
$\dot{m}$	55,300	5,533	700
Specific Impulse	230	286	286

04001016  
G. Yashwanth.

Payload =  
35400 kg.

Part (a): Find Burnout velocity

$$V_f = - \sum_{i=1}^3 v_{ci} \ln(\epsilon_i + (1-\epsilon_i)\pi_i)$$

$$v_{c1} = 230 \text{ g}$$

$$v_{c2} = 286 \text{ g}$$

$$v_{c3} = 286 \text{ g}$$

$$\epsilon_1 = \frac{6,98,390}{6,98,390 + 47,61,750} = 0.1279$$

$$\epsilon_2 = \frac{69840}{69840 + 698400} = 0.0909$$

$$\epsilon_3 = \frac{21950}{69480 + 21950} = 0.2401$$

$$\pi_3 = \frac{35400}{35400 + 21950 + 69480} = \frac{35400}{126830} = 0.2791$$

$$\pi_2 = \frac{126830}{126830 + 69840 + 698400} = 0.1417$$

$$\pi_1 = \frac{895070}{895070 + 698390 + 47,61,750} = 0.1408$$

$$\therefore V_f = 230g \times 1.38553 + 286g \times 1.1514 + 286g \times 0.7936$$

$$= 9590 \text{ m/sec}$$

Burnout Velocity = 9590 m/sec

(b) Structural mass increased by 7% in stage 2 & 3  
 Specific Impulse is 295

Assuming that mass of propellant remains same.

Let new payload be  $m^* = P$

$\Pi_3 = \frac{P}{P + 92966}$	$m_s$	Stage 1	Stage 2	Stage 3
	$m_p$	698590	74728	23486
		4761750	698400	69480

$$\Pi_2 = \frac{P + 92966}{P + 866094}$$

$$\epsilon_1 = 0.1279$$

$$\epsilon_2 = 0.0966$$

$$\epsilon_3 = 0.2526$$

$$\Pi_{1,2} = \frac{P + 866094}{P + 6326234}$$

$$9590 = - \left[ 230g \ln(\epsilon_1 (1 - \epsilon_1) \Pi_1) + 295g \ln(\epsilon_2 + (1 - \epsilon_2) \Pi_2) + 295g \ln(\epsilon_3 (1 - \epsilon_3) \Pi_3) \right]$$

Substituting  $\epsilon_1, \epsilon_2, \epsilon_3, \Pi_1, \Pi_2, \Pi_3$  from above and solving, we get  $P = 37611 \text{ kg}$

$\therefore$  Increase in Payload =

$$= \underline{\underline{2211 \text{ kg}}}$$

37611
35400
<hr/>
2211

how did you solve this?

YOU HAVE TO USE

TRADE-OFF

RATIOS FOR THIS PROBLEM

(c) Velocity Increment for last two stages =

$$V_{f3} - V_{f1} = (V_{f3} - V_{f2}) + (V_{f2} - V_{f1})$$

$$= 9590 - 3118 = \underline{\underline{6472 \text{ m/sec}}}$$

Re design - third stage

let structural mass be  $m_{s3}$

let propellant mass be  $m_{p3}$

overall payload ratio for last two stage =  $\Pi_2 \Pi_3$

$$\Pi_2 \Pi_3 = \frac{m^+}{(m_{s2} + m_{p2}) + m_{s3} + m_{p3} + m^+} \rightarrow \text{maximize}$$

given:  $\frac{m_{s2}}{m_{p2} + m_{s2}} = \frac{m_{s3}}{m_{s3} + m_{p3}} = \frac{1}{11}$

$\Rightarrow m_{s3} + m_{p3} = 11 m_{s3} \Rightarrow m_{p3} = 10 m_{s3}$

$\Rightarrow$  maximize  $\frac{m^+}{768240 + 11 m_{s3} + m^+}$

subject to:

$$V_{f3} - V_{f1} = -V_{e3} \ln(\epsilon_3 + (1 - \epsilon_3) \Pi_3) - V_{e2} \ln(\epsilon_2 + (1 - \epsilon_2) \Pi_2)$$

" " " " " "

$$6472 = -2869 \ln$$

$$\epsilon_3 = \frac{m_{s3}}{m_{s3} + m_{p3}} = \frac{1}{11}$$

$$\Pi_3 = \frac{m^+}{11 m_{s3} + m^+}$$

$$\epsilon_2 = \frac{1}{11}$$

$$\Pi_2 = \frac{11 m_{s3} + m^+}{(11 m_{s3} + m^+) + 768240}$$

Simply  
You have to use the  
solution for the ~~optimal~~  
optimally staged  
rocket that  
we derived in  
class.

$$6472 = -2869 \ln \left[ \frac{0.0909 + 0.9091 \times (11m_{S_2} + m^+)}{(11m_{S_2} + m^+ + 768240)} \right]$$

$$-2869 \ln \left[ \frac{0.0909 + 0.9091 \times \frac{m^+}{11m_{S_2} + m^+}}{11m_{S_2} + m^+} \right]$$

12/3/08. Soln. to tutorial problems.

MAYUR SINGH  
040101003

But the problem has a parallel burning phase,

Q. 37 → In ideal condition, there is no overlapping of stages.

Let us assume vehicle ascent at constant thrust during a stage and under uniform gravity. → for maximum possible burnout speed, assume gravity = 0. for maximum burnout speed of PSLV, thrust should be maintained constant = max. thrust of each stage.

The final burnout speed after 4<sup>th</sup> stage

$$v_b = v_{b3} + [-g t_{b4} + v_{e4} \ln \left( \frac{m_{i4}}{m_{f4}} \right)]$$

x x  $m_{b4} = m_4 + m_{s4}$ .

$m_{f4} = m_x$  = for payload weight

Similarly,

$$v_{b3} = v_{b2} + [-g t_{b3} + v_{e3} \ln \left( \frac{m_{i3}}{m_{f3}} \right)]$$

$$v_{b2} = v_{b1} + [-g t_{b2} + v_{e2} \ln \left( \frac{m_{i2}}{m_{f2}} \right)]$$

$$v_{b1} = v_L + [-g (t_{b1} - t_{b0}) + v_{e1} \ln \left( \frac{m_{i1}}{m_{f1}} \right)]$$

$$v_1 = 0 - g t_{b0} + \bar{v}_e \ln \left( \frac{m_i}{m_f} \right)$$

g! where  $t_{b0}$  → burnout time for booster

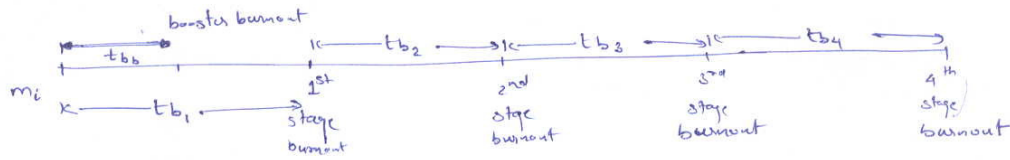
&  $\bar{v}_e$  = equivalent relative exit velocity

$$= \frac{G \cdot \dot{m}_b \cdot v_{eb} + \dot{m}_1 \cdot v_{e1}}{\dot{m}_b + \dot{m}_1}$$

~~$m_f = m_{i1}, m_{f1} = m_{i2}$~~

$$m_* = (1050 + 107 + 45) \text{ kg} = 1202 \text{ kg}$$

$$m_i = m_* + m_{p_1} + m_{s_1} + m_{p_2} + m_{s_2} + m_{p_3} + m_{s_3} + m_{p_4} + m_{s_4}$$



$$m_i = (1202 + 229 + 46 + 8.4 + 2.89) \text{ ton} \quad \left. \vphantom{m_i} \right\} \text{ for which stage?}$$

$$m_i = 287.492 \text{ ton}$$

$$m_f = \text{mass taken after } t_{b_b}$$

$$= m_i - \cancel{m_{p_1}} + m_{p_1} \cdot (t_{b_1} / t_{b_b})$$

$$= 287.492 - \frac{138}{107.4} \cdot (107.4 + 45) - 54$$

$$m_f = \cancel{207.313 \text{ ton}} \quad \cancel{229.67 \text{ ton}} \quad 175.67 \text{ ton}$$

$$V_{e_b} = \frac{T_b}{\dot{m}_b} = \frac{662 \times 45}{9} = 3310 \text{ m/sec}$$

$$V_{e_1} = \frac{T_1}{\dot{m}_p} = \frac{4628 \times 107.4}{138} = 3601.79 \text{ m/sec}$$

$$\bar{V}_e = \frac{6 \cdot T_b + T_1}{\dot{m}_p + \dot{m}_b} = \frac{6 \times 662 + 4628}{\frac{9}{45} + \frac{138}{107.4}} = 5791.57 \text{ m/sec}$$

$$\Rightarrow V_i = -9.8 \times 45 + 5791.57 \ln \left( \frac{287.492}{\cancel{229.67}} \right) \ln \left( \frac{287.492}{175.67} \right)$$

$$V_i = \cancel{1452.64 \text{ m/sec}}$$

$$V_i = \cancel{859.5 \text{ m/sec}} \quad V_i = 2411.86 \text{ m/sec}$$

$$m_{i1} = m_i - m_{pb} - m_{p1} \times t_b = m_f$$

$$= 175.67 \text{ ton}$$

$$m_{f1} = m_i - m_{pb} - m_{i1}$$

$$= 287.492 - 54 - 138$$

$$= 95.492 \text{ ton}$$

$v_{b1} \Rightarrow$  Burnout velocity <sup>speed</sup> after 1<sup>st</sup> stage

$$v_{b1} = v_1 + \left[ -g(t_{b1} - t_{b0}) + v_{e1} \ln \left( \frac{m_{i1}}{m_{f1}} \right) \right]$$

$$= 2411.86 + \left[ 9.8(107.4 - 45) + 3601.79 \ln \left( \frac{175.67}{95.492} \right) \right]$$

$$v_{b1} = 3995.86 \text{ m/sec}$$

~~Burnout velocity after~~

Burnout speed of 2<sup>nd</sup> stage

$$v_{b2} = v_{b1} - g t_{b2} + v_{e2} \ln \left( \frac{m_{i2}}{m_{f2}} \right)$$

$$t_{b2} = 163 \text{ sec}$$

$$v_{e2} = \frac{725}{40.6} \times 163$$

$$= 2910.71 \text{ m/sec}$$

$$m_{i2} = m_i - (m_{p1} + m_{pb} + m_{s1} + m_{s2}) = m_f - m_{s1} - m_{s2}$$

$$= 287.492 - 229$$

$$= 58.492 \text{ ton}$$

$$m_{f2} = m_i - m_{i2} - m_{p2}$$

$$= 58.492 - 40.6$$

$$= 17.892 \text{ ton}$$

$$\Rightarrow V_{b2} = 3995.86 - 9.8 \times 163 + 2910.91 \ln \left( \frac{58.492}{17.892} \right)$$

$$V_{b2} = 5846.30 \text{ m/sec}$$

$$V_{b3} = V_{b2} - g t_{b3} + V_{e3} \ln \left( \frac{m_{i3}}{m_{f3}} \right)$$

$$t_{b3} = 76 \text{ sec}$$

$$V_{e3} = \frac{340}{7.2} \times 76$$

$$= 3588.89 \text{ m/sec}$$

$$m_{i3} = m_{j2} - m_{b2}$$

$$= 58.492 - 46$$

$$= 12.492 \text{ ton}$$

$$m_{f3} = m_{i3} - m_{p3}$$

$$= 12.492 - 7.2$$

$$= 5.292 \text{ ton}$$

$$V_{b3} = \frac{3588.89}{5846.30} - 9.8 \times 76 + 3588.89 \ln \left( \frac{12.492}{5.292} \right)$$

$$= 8183.96 \text{ m/sec}$$

$$V_b = V_{b4} = V_{b3} - g t_{b4} + \bar{V}_{e4} \ln \left( \frac{m_{i4}}{m_{f4}} \right)$$

$$\bar{V}_{e4} t_{b4} = 415 \text{ sec}$$

there are 2 engines in 4<sup>th</sup> stage

i.e. parallel combustion

1 ton each in each

$$\dot{m} = \frac{14.8 \times 415}{2}$$

$$\bar{V}_{e4} = \frac{2 \times \dot{m} V_{e4}}{\dot{m} + \dot{m}} = V_{e4}$$

$$= \frac{14.8 \times 415}{2} = 3071 \text{ m/sec}$$



$$\begin{aligned}
 m_{i4} &= m_{f3} - m_{s3} \\
 &= 12.492 - 8.4 \\
 &= 4.092
 \end{aligned}$$

$$\begin{aligned}
 m_{f4} &= m_{i4} - m_{p4} \\
 &= 4.092 - 2 \\
 &= 2.092
 \end{aligned}$$

$$\begin{aligned}
 \Rightarrow V_{b4} = V_b &= 8183.96 - 9.8 \times 415 + 3071 \ln \left( \frac{4.092}{2.092} \right) \\
 &= 6177.33 \text{ m/sec}
 \end{aligned}$$

As it after observing burnout speed of each stage  
 it is clear that maximum burnout speed is of  
 3<sup>rd</sup> stage

$$\text{i.e. } (V_b)_{\max} = V_{b3} = \underline{8183.96 \text{ m/sec}}$$

This is not what is meant.

Maximum possible injection speed of  
 the payload is asked.

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Jyoti J. Malgundkar

\* First stage - GS1 :

$$m_{j1} = m_{s1} + m_{p1} + m_{j2}$$

$$m_{f1} = m_{s1} + m_{j2}$$

$m_{s1}$  = total structural mass of solid stage (S125)  
plus that of four L40 boosters strapped on  
to S125

$m_{p1}$  = total propellant mass of S125 and 4 L40 boosters

$$\therefore m_{s1} = (156 - 129) + 4(46 - 40) = 51 \text{ tonnes} = 51 \times 10^3 \text{ kg}$$

$$m_{p1} = 129 + (4 \times 40) = 289 \text{ tonnes} = 289 \times 10^3 \text{ kg}$$

\* Second stage - GS2 :

$$m_{j2} = m_{s2} + m_{p2} + m_{j3}$$

$$m_{f2} = m_{s2} + m_{j3}$$

↓ not correct. S125 burns for 100 sec.  
L40s burn for 160 sec.  
Both are ejected together.  
You have to treat 60 sec.  
separately.!

Total mass = 42.8 tonnes      propellant mass = 38 tonnes

$$\therefore m_{p2} = 38 \text{ tonnes} = 38 \times 10^3 \text{ kg}$$

$$m_{s2} = (42.8 - 38) = 4.8 \text{ tonnes} = 4.8 \times 10^3 \text{ kg}$$

2nd stage burns 38 tonnes of propellant in 150 to 60 sec

\* Third stage - GS3 :

$$m_{j3} = m_{s3} + m_{p3} + m^*$$

$$m_{f3} = m_{s3} + m^*$$

Total mass = 15 tonnes      propellant mass = 12.5 tonnes

$$\therefore m_{p3} = 12.5 \text{ tonnes} = 12.5 \times 10^3 \text{ kg}$$

$$m_{s3} = (15 - 12.5) = 2.5 \text{ tonnes} = 2.5 \times 10^3 \text{ kg}$$

$$m^* = 1530 \text{ kg}$$

$$\therefore m_{i3} = (2500 + 12500 + 1530) = 16530 \text{ kg}$$

$$m_{f3} = 2500 + 1530 = 4030 \text{ kg}$$

$$m_{i2} = (88000 + 4800 + 16530) = 59330 \text{ kg}$$

$$m_{f2} = 21330 \text{ kg}$$

$$m_{i1} = 399,330 \text{ kg}$$

$$m_{f1} = 110,330 \text{ kg}$$

\* To find relative exit velocity at each stage

$$1^{\text{st}} \text{ stage} \rightarrow F_{\text{net}} = F_{125} + 4 F_{140}$$

$$\dot{m}_{\text{tot}} \bar{V}_{e1} = 4700 + (4 \times 680) = 7420 \text{ kN}$$

$$\dot{m}_{\text{tot}} = \left( \frac{129}{102} \times 10^3 + 4 \times \frac{90 \times 10^3}{160} \right)$$

$$= 10^3 (1.29 + 1) = 2.29 \times 10^3 \text{ kg/sec}$$

$$2.29 \times 10^3 \bar{V}_{e1} = 7420 \times 10^3 \text{ N}$$

$$\boxed{\bar{V}_{e1} = 3240.17 \text{ m/sec.}}$$

$$2^{\text{nd}} \text{ stage} \rightarrow V_{e2} = \frac{F_2}{\dot{m}_2} = \frac{720 \times 10^3}{\left( \frac{88 \times 10^3}{150} \right)}$$

$$\boxed{V_{e2} = 2842.10 \text{ m/sec.}}$$

$$3^{\text{rd}} \text{ stage} \rightarrow v_{e3} = \frac{F_3}{m_3} = \frac{78.5 \pi 10^3}{\left(\frac{12.5 \times 10^3}{720}\right)}$$

$$\boxed{v_{e3} = 4233.6 \text{ m/sec}}$$

$$\text{Now } v_f = \sum_{k=1}^3 v_{ek} \ln \left( \frac{m_{ik}}{m_{fk}} \right)$$

$$= 8240.17 \ln \left( \frac{399830}{110,330} \right) + 2842.10 \ln \left( \frac{59330}{21830} \right) \\ + 4233.6 \ln \left( \frac{16530}{4080} \right)$$

$$v_f = 4107.87 + 2907.46 + 5975.34$$

$$\boxed{v_f = 13050.67 \text{ m/sec}}$$

Problem # 42

T. Sateesh

03001017

$$V_f = \sum V_{ej} \ln \left[ \frac{m_{ij}}{m_{fj}} \right]$$

$$m_{ij} = m^* + m_{pj} + m_{sj} + \sum_{i=j+1}^N (m_{si} + m_{pi})$$

$$m_{fj} = m^* + 0 + m_{sj} + \sum_{i=j+1}^N (m_{si} + m_{pi})$$

$$\frac{\partial m^*}{\partial V_{ej}} = - \frac{\partial V_f / \partial V_{ej}}{\partial V_f / \partial m^*} \quad (\text{partial derivatives rules})$$

$$\left\{ \frac{\partial V_f}{\partial V_{ej}} = \sum_j \ln \left[ \frac{m_{ij}}{m_{fj}} \right] \right. \quad \left. \left\{ \text{(the summation of all those where exit vel. is changed)} \right\} \right.$$

$$\left. \left\{ \frac{\partial V_f}{\partial m^*} = \sum_{j=1}^N V_{ej} \left[ \frac{1}{m_{ij}} - \frac{1}{m_{fj}} \right] \right. \right.$$

$$\left. \Rightarrow \frac{\partial m^*}{\partial V_e} = \frac{\sum \ln \left[ \frac{m_{ij}}{m_{fj}} \right]}{\sum_{j=1}^N V_{ej} \left[ \frac{1}{m_{ij}} - \frac{1}{m_{fj}} \right]} \right.$$

$$m_{p1} = 1167 \text{ kg}, \quad m_{s1} = 113 \text{ kg}$$

$$m_{p2} = 415 \text{ kg}, \quad m_{s2} = 41 \text{ kg}$$

$$m^* = 150 \text{ kg}$$

$$I_{sp} = 282 \text{ sec}; \quad \Delta I_{sp} = 10 \text{ s.}$$

$$g \cdot I_{sp} = V_e \Rightarrow V_e > 282 \times 9.8 = 2763.6 \text{ m/s}$$

$$\frac{\partial m^*}{\partial V_e}$$

$$m_{1i} = 1167 + 113 + 415 + 41 + 150 = 1886 \text{ kg}$$

$$m_{1f} = 1167 + 113 + 415 + 41 + 150 = 719 \text{ kg}$$

$$m_{2i} = 415 + 41 + 150 = 606 \text{ kg}$$

$$m_{2f} = 150 + 41 = 191 \text{ kg}$$

suppose  $I_{sp}$  for 1st stage is changed, by 10 s improved

$$\frac{\partial m^*}{\partial V_e} = \frac{\ln \left[ \frac{1886}{719} \right]}{2763.6 \left\{ \left( \frac{1}{1886} - \frac{1}{719} \right) + \left( \frac{1}{606} - \frac{1}{191} \right) \right\}}$$

$$\Rightarrow \frac{\partial m^*}{\partial v_e} = 0.7845$$

$$\begin{aligned}\Rightarrow \Delta m^* &= 0.7845 \times \Delta v_e \\ &= 0.7845 \times 10 \times 9.8 \\ &= 76.8 \text{ kg}\end{aligned}$$

Suppose 2<sup>nd</sup> stage is improved by 10s (Isp)

$$\begin{aligned}\frac{\partial m^*}{\partial v_e} &= -\ln \left[ \frac{606}{9191} \right] \\ &= 2.763 \left\{ \left[ \frac{1}{1886} - \frac{1}{719} \right] + \left[ \frac{1}{606} - \frac{1}{191} \right] \right\} \\ &= 0.939693\end{aligned}$$

$$\begin{aligned}\Rightarrow \Delta m^* &= 0.939693 \times 10 \times 9.8 \\ &= 92.0899 \text{ kg}\end{aligned}$$

It is better to make the specific impulse change in second stage.